For Help Desk Phone Numbers Click here

# **Selected Model**

Engine: 3412 **Generator Frame: 592**  Genset Rating (kW): 550.0 Line Voltage: 480

Fuel: Diesel

Generator Arrangement: 1366634 Genset Rating (kVA): 687.0 Phase Voltage: 277

Frequency: 60 Excitation Type: Permanent Magnet Pwr. Factor: 0.8 Rated Current: 826.3

Version: 39094/38912/38261/2609

**Duty: STANDBY Connection: SERIES STAR** 

**Application:** EPG Status: Current

# **Spec Information**

Generator Specific	ation	Generator Efficiency		
Frame: 592 Type: SR4B	No. of Bearings: 1	Per Unit Load	kW	Efficiency %
Winding Type: RANDOM WOUND Connection: SERIES STAR	Housing: 0	0.25	137.5	91.9
Phases: 3	No. of Leads: 12	0.5	275.0 412.5	94.3 94.4
Poles: 4	Wires per Lead: 2	1.0	550.0	94.4
Sync Speed: 1800	<b>Generator Pitch:</b> 0.8			

Reactances	Per Unit	Ohms
SUBTRANSIENT - DIRECT AXIS X" <sub>d</sub>	0.2020	0.0677
SUBTRANSIENT - QUADRATURE AXIS $X''_q$	0.1969	0.0660
TRANSIENT - SATURATED $X'_d$	0.2888	0.0968
SYNCHRONOUS - DIRECT AXIS $X_d$	3.7813	1.2672
SYNCHRONOUS - QUADRATURE AXIS $X_{\mathfrak{q}}$	1.9249	0.6451
NEGATIVE SEQUENCE $X_2$	0.1996	0.0669
ZERO SEQUENCE $X_0$	0.0919	0.0308
Time Constants		Seconds
OPEN CIRCUIT TRANSIENT - DIRECT AXIS T'd0	2.3980	
SHORT CIRCUIT TRANSIENT - DIRECT AXIS T'd	0.1832	
OPEN CIRCUIT SUBSTRANSIENT - DIRECT AXIS T" <sub>d0</sub> 0.0091		
SHORT CIRCUIT SUBSTRANSIENT - DIRECT AXIS T" <sub>d</sub> 0.0069		
OPEN CIRCUIT SUBSTRANSIENT - QUADRATURE AXIS T" <sub>q0</sub> 0.0069		
SHORT CIRCUIT SUBSTRANSIENT - QUADRATURE AX	XIS T" <sub>q</sub>	0.0076
EXCITER TIME CONSTANT T <sub>e</sub>	0.1400	
ARMATURE SHORT CIRCUIT T <sub>a</sub>		0.0278
Short Circuit Ratio: 0.34 Stator Resistance = 0.0122 Ohms	s Field Resistar	nce = 1.27 Ohms

Voltage Regulation			Generator Excit	ation	
Voltage level adjustment: +/-	5.0%		No Load	Full Load, (r	ated) pf
Voltage regulation, steady state: +/-	0.5%			Series	Parallel
Voltage regulation with 3% speed change: +/-	0.5%	Excitation voltage:	7.58 Volts	43.85 Volts	Volts
Waveform deviation line - line, no load: less than	5.0%	<b>Excitation current</b>	1.68 Amps	8.0 Amps	Amps
Telephone influence factor: less than	50				

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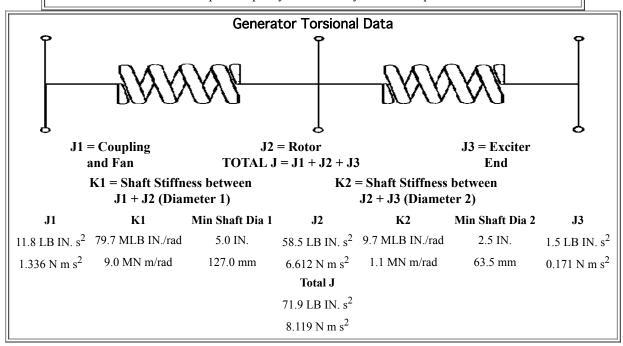
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#### **Generator Mechanical Information**

Center of Gravity			
Dimension X	-646.4 mm	-25.4 IN.	
Dimension Y	0.0 mm	0.0 IN.	
Dimension Z	0.0 mm	0.0 IN.	

- "X" is measured from driven end of generator and parallel to rotor. Towards engine fan is positive. See General Information for details
- "Y" is measured vertically from rotor center line. Up is positive.
- "Z" is measured to left and right of rotor center line. To the right is positive.

Rotor Balance = 0.0508 mm deflection PTP Overspeed Capacity = 150% of synchronous speed



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# Generator Cooling Requirements -Temperature - Insulation Data

Cooling Requirements: Temperature Data: (Ambient 40 <sup>0</sup>C)

**Heat Dissipated:** 35.1 kW **Stator Rise:**  $130.0 \, ^{0}\text{C}$  **Air Flow:**  $112.2 \, \text{m}^{3}/\text{min}$  **Rotor Rise:**  $130.0 \, ^{0}\text{C}$ 

**Insulation Class: H** 

**Insulation Reg. as shipped:**  $100.0 \text{ M}\Omega$  minimum at  $40 \, ^{0}\text{C}$ 

# Thermal Limits of Generator

Frequency: 60 Hz
Line to Line Voltage: 480 Volts
B BR 80/40 519.0 kVA
F BR -105/40 625.0 kVA
H BR - 125/40 688.0 kVA
F PR - 130/40 688.0 kVA

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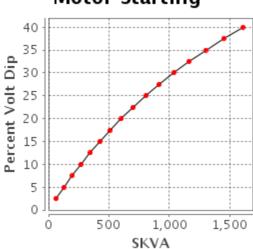
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# Starting Capability & Current Decrement Motor Starting Capability (0.4 pf)

SKVA	Percent Volt Dip
62	2.5
127	5.0
196	7.5
268	10.0
345	12.5
426	15.0
512	17.5
603	20.0
701	22.5
805	25.0
916	27.5
1,034	30.0
1,162	32.5
1,300	35.0
1,448	37.5
1,609	40.0

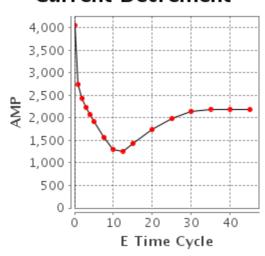
# **Motor Starting**



#### **Current Decrement Data**

E Time Cycle	AMP
0.0	4,060
1.0	2,747
2.0	2,439
3.0	2,241
4.0	2,068
5.0	1,910
7.5	1,573
10.0	1,305
12.5	1,262
15.0	1,431
20.0	1,745
25.0	1,979
30.0	2,151
35.0	2,197
40.0	2,194
45.0	2,185

# **Current Decrement**



**Instantaneous 3 Phase Fault Current: 4060 Amps** 

**Instantaneous Line - Line Fault Current:** 3539 Amps

**Instantaneous Line - Neutral Fault Current:** 4989 Amps

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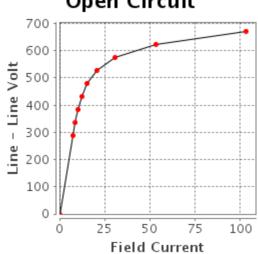
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# **Generator Output Characteristic Curves Open Circuit Curve**

# Open Circuit

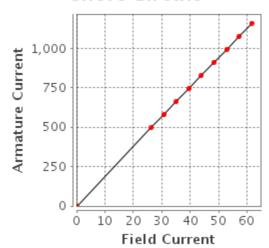
Field Current	Line - Line Volt
0.0	0
7.4	288
8.8	336
10.3	384
12.3	432
15.3	480
20.5	528
30.9	576
53.3	624
103.2	672



## **Short Circuit Curve**

# **Short Circuit**

Field Current	Armature Current
0.0	0
26.4	496
30.8	579
35.2	662
39.6	744
44.0	827
48.4	910
52.9	992
57.3	1,075
61.7	1,158



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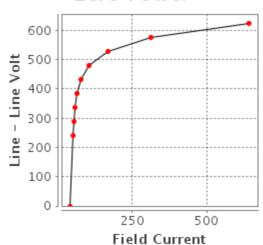
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# Generator Output Characteristic Curves Zero Power Factor Curve

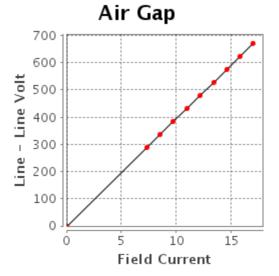
# Zero Power

Field Current	Line - Line Volt
44.0	0
54.3	240
56.5	288
59.9	336
66.2	384
79.0	432
106.9	480
169.6	528
312.4	576
639.2	624



# Air Gap Curve

Field Current	Line - Line Volt
0.0	0
7.3	288
8.5	336
9.7	384
11.0	432
12.2	480
13.4	528
14.6	576
15.8	624
17.0	672



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# Reactive Capability Curve Operating Chart

# Leading Lagging 1.2 0/.8 PF 0.8 A 1.0 PF **Engine Limit** kW/ Rated kVA 0.6 PE/ Q.6 PF 0.6 Q4 PF 0.4 BF 0.4 0.2 PF 0.2 PF -1 -0.8 -0.6 -0.4Ó 0.4 0.6 0.8 1 kVAr/ Rated kVA

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#### **General Information**

DM7802

GENERATOR GENERAL INFORMATION

I. GENERATOR MOTOR STARTING CAPABILITY CURVES
A. THE MOTOR STARTING CURVES ARE REPRESENTATIVE OF THE DATA
OBTAINED BY THE FOLLOWING PROCEDURE:

- 1. THE CATERPILLAR GENERATOR IS DRIVEN BY A SYNCHRONOUS DRIVER.
- 2. VARIOUS SIZE THREE PHASE INDUCTION MOTORS (NEMA CODE F) ARE STARTED ACROSS THE LINE LEADS OF THE UNLOADED GENERATOR.
- 3. THE RESULTING VOLTAGE DIPS ARE RECORDED WITH AN OSCILLOSCOPE.
- 4. MOTOR HORSEPOWER HAS BEEN CONVERTED TO STARTING KILOVOLT AMPERES (SKVA).
- 5. RECORDED VOLTAGE DIPS HAVE BEEN EXPRESSED AS A OF GENERATOR RATED VOLTAGE.

II. USE OF THE MOTOR STARTING CAPABILITY CURVES.

A. CALCULATE THE SKVA REQUIRED BY THE MOTOR FOR FULL VOLTAGE STARTING ACROSS THE LINE IF THE VALUE IS NOT LISTED ON THE MOTOR DATA PLATE.

1. MOTORS CONFORMING TO NEMA STANDARDS MULTIPLY THE MOTOR HORSEPOWER BY THE NEMA SKVA/HP FIGURE. FOR NEMA CODE F,USE 5.3 SKVA/HP; FOR NEMA CODE G, USE 6.0 SKVA/HP.

2. ALL OTHER MOTORS:

MULTIPLY THE RATED VOLTAGE BY THE LOCKED ROTOR AMPERE AND BY 0.001732. (IF THE LOCKED ROTOR AMPERES ARE NOT LISTED, MULTIPLY THE FULL LOAD (RUNNING) AMPERES BY B. USE THE ABOVE SKVA WITH THE MOTOR STARTING TABLE.

1. ACROSS LINE STARTING:

READ ACROSS THE ROW OF "ACROSS THE LINE STARTING SKVA IF THE DESIRED VALUE OF SKVA IS NOT GIVEN, CALCULATE THE DIP BY FINDING THE PROPER SKVA INTERVAL AND INTERPOLATING AS FOLLOWS:

SKVA1 IS THE SKVA TABLE ENTRY JUST SMALLER THAN THE DESIRED SKVA, DIP1 IS THE DIP FOR SKVA2, AND SKVA2 IS THE SKVA TABLE ENTRY JUST GREATER THAN THE DESIRED SKVA. THE DIP (IN PERCENT) AT THE DESIRED SKVA IS:

DIP = DIP1 + (SKVA - SKVA1) \* 2.5 /

(SKVA2 - SKVA1)

NOTE: VOLTAGE DIPS GREATER THAN 35% MAY CAUSE MAGNETIC CONTACTORS TO DROP OUT.

#### 2. REDUCED VOLTAGE STARTING:

REFER TO THE FOLLOWING TABLE. MULTIPLY THE CALCULATE ACROSS LINE SKVA BY THE MULTIPLIER LISTED FOR THE SPECIFIC STARTING METHOD. APPLY THE RESULT TO THE STARTING TABLE AS IN II A, TO CALCULATE THE EXPECTED VOLTAGE DIP:

TYPE OF REDUCED MULTIPLY
VOLTAGE STARTING LINE SKVA BY
80% TAP .60
65% TAP .65
50% TAP .50
45% TAP .45

#### AUTOTRANSFORMER

80% TAP .68 65% TAP .46 50% TAP .29

Wye start, delta run .33

NOTE: REDUCE VOLTAGE STARTING LOWERS THE MAXIMUM

#### REQUIRED MOTOR skVA.

3. Part winding starting:

Most common is half-winding start, full-winding run. Multiply the full motor, accross line starting skVA by 0.6. Apply the result to the selected curve as in ii. A above. Read the expected voltage dip, for the required skVA.

#### III.DEFINITION:

A. GENERATOR TERMS

 $\begin{aligned} & \text{MODEL:} & \text{Engine Sales model} \\ & \text{ENG TYPE:} & & \text{DI = Direct Injection,} \end{aligned}$ 

NA = Naturally aspirated, etc HZ: Running frequency, hertz

RATING TYPE: PP, SB (prime power or standby) KW: Base rating electrical kilowatts (ekW)

VOLTS: Rating terminal, line to line

GEN ARR: Cat generator arrangement part number GEN FRAME: Generator frame size designation

CONN: Generator output connection

(star, wye, delta, ect.)

POLES: Number of pole pieces on rotor.

(eg. A 4 pole generator run at 1800)

RPM will produce 60 Hz alternating current. A 6 pole generator run at 1200 RPM will produce 60 Hz alternating current.)

#### B. GENERATOR TEMPERATURE RISE:

The indicated temperature rise indicated the NEMA limits for standby or prime power applications. These rises are used for calculating the losses and efficiencies and are not necessarily indicative of the actual temperature rise of a given machine.

#### C. CENTER OF GRAVITY

The specified center of gravity is for the generator only. For single bearing, and two bearing close coupled generators, the cent er of gravity is measured from the generator/engine flywheel housing i nterface and from the centerline of the rotor shaft.

For two bearing, standalone generators, the center of gravity is measu red from the end of the rotor shaft and from the centerline of the rot or shaft.

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#### D. GENERATOR DECREMENT CURRENT CURVES

The generator decrement current curve gives the symmetrical current supplied by the generator for a three phase bolted fault at the generator terminals. Generators equipped with the series boost attachment or generators with PM excitation system will supply 300% of rated current for at least 10 seconds.

#### E. GENERATOR EFFICIENCY CURVES

The efficiency curve is representative of the overall generator efficiency over the normal range of the electrical load and at the specified parameters. This is not the overall engine generator set efficiency curve.

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